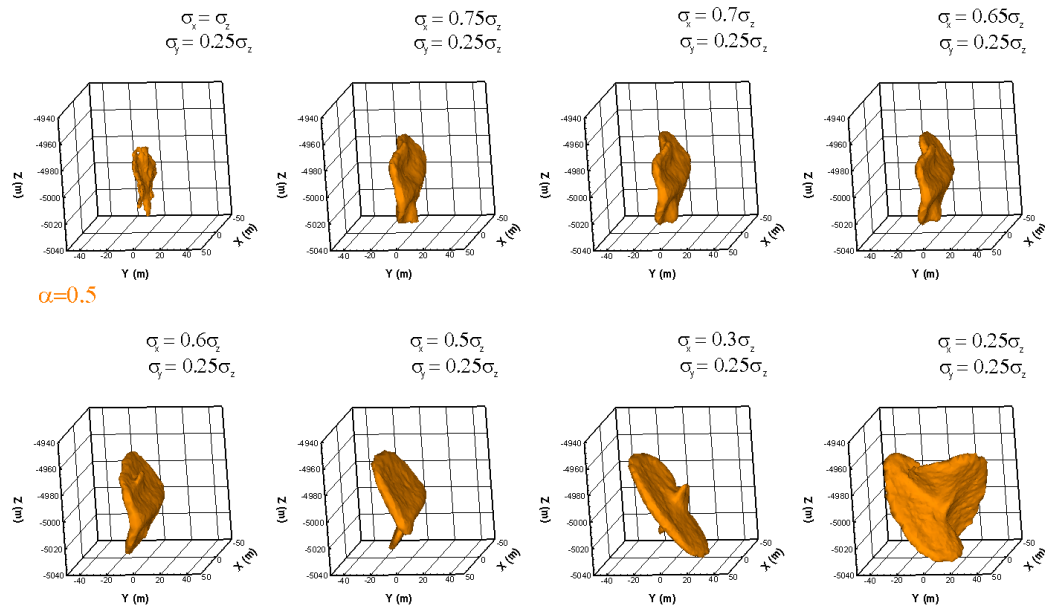


**THE ROLE OF THE INTERMEDIATE STRESS ON FAILURE DIRECTION**

E. Shalev<sup>1</sup> & V. Lyakhovsky<sup>1</sup>  
<sup>1</sup>Geological Survey of Israel, Jerusalem, Israel

Key words fault direction, damage.

The directions of faults are often suggested to correspond to the Coulomb failure criterion. In these analyses, only the maximum ( $\sigma_1$ ) and least principle ( $\sigma_3$ ) stresses control fault formation and their orientation. However, it has been demonstrated that the intermediate stress ( $\sigma_2$ ) plays a major role in rock failure and that the Coulomb failure criterion is not accurate under true 3-D loading conditions. Alternative criteria for failure, as Drucker-Prager, Wiebols-Cook, Hoek-Brown, Lade, Mogi and others were suggested to include all stress components but did not attempt to predict the direction of failure with respect to the principle stress orientation. We numerically simulate rock failure using damage-rheology mechanical model that describes the accumulation of damage intensity as a function of the ongoing deformation that eventually leads to macroscopic brittle failure. Our criterion for the onset of damage accumulation is described as  $\xi = I_1/\sqrt{I_2} > \xi_0$ , where  $I_1$  and  $I_2$  are the first and second strain invariants, and  $\xi_0$  is the critical strain invariants ratio which corresponds to the internal friction in the stress failure models. We run a set of simulations in which only  $\sigma_2$  is varied between simulations while  $\sigma_1$  and  $\sigma_3$  remain the same. Nucleation and propagation of the faults were driven by fluid injection at the center of the simulated rock volume. Results show that the angle between the fault and  $\sigma_1$  changes from oblique ( $\sim 35^\circ$ ) at  $\sigma_2=\sigma_3$  to vertical ( $0^\circ$ ) at  $\sigma_2=\sigma_1$  (figure 1). Although all local failure were in shear mode of deformation and there was no tensile stress in the systems, the nearly vertical fault structure at  $\sigma_2=\sigma_1$  is similar to tension regime or axial splitting. Keeping  $\sigma_1$  and  $\sigma_3$  constants and increasing the intermediate stress component from low values  $\sigma_2=\sigma_3$  to  $\sigma_2=\sigma_1$  significantly affects the proximity to failure. The mean stress ( $\sigma_m=(\sigma_1+\sigma_2+\sigma_3)/3$ ) increases with  $\sigma_2$ , while the differential stress ( $\sigma_1-\sigma_3$ ) remains the same. This stabilizes the rock and drives the state of stress farther from failure conditions. Therefore, stress shadowing that promotes only one conjugate direction is more significant at low intermediate stress values. At high intermediate stresses shadowing is weak and both conjugate directions are constantly active giving an average vertical fault direction. Interpreting fault patterns without considering the intermediate stress can lead to wrong conclusions regarding stress directions and failure mechanisms.



**Figure 1.** Iso-damage ( $a=0.5$ ) surfaces for the simulated faults.  $\sigma_1$  and  $\sigma_3$  are the same for all cases. Direction of faults change with respect to  $\sigma_2$ .